

# The evolution of Drift Chambers at e<sup>+</sup>e<sup>-</sup> Colliders

(lessons learnt from a ≥40-years long experience)

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**INSTR2020**  
BINP, Novosibirsk

INSTR20: Instrumentation for Colliding Beam Physics  
Budker Institute of Nuclear Physics, Novosibirsk, Russia  
24 - 28 February, 2020

# Outline of the talk

## ➤ Performance evolution

- Momentum Resolution
- $dE/dx$ ,  $dN/dx$  and  $Pl_d$
- Mechanical Structure ( $X_0$ )
- FE and RO Electronics → NOT NOW

## ❖ Only Cylindrical Drift Chambers

- No **Planar** Drift Chambers
- No **Time Projection** Chambers
- No **Time Expansion** Chambers
- No **Radial** Drift Chambers:  
radial wires – H1-forward/HERA  
radial drift – ASTERIX/CERN
- No **Straw Tube** Cyl. Chambers (GlueX, PANDA)

## ❖ Only $e^+e^-$ colliders

- No **fixed target** configurations (MEG2)
- No **ep and pp colliders** (AFS, CDF-CTC/COT)

## ❖ Layout Evolution

- From **single** sense wire cell, to **multiple** sense wires and **jet** cell configurations - and back to **single** sense wire cell
- **Axial-stereo** and **full stereo** layer configuration (KLOE, 4<sup>th</sup>-Concept, MEG2, IDEA)

## ❖ Gas mixture Evolution

- From **Argon** to **Helium** based gas

## ❖ Mechanical Structure and Wires Evolution

**Read-out: from first clusters timing to Cluster Counting and Cluster Timing**

# Trackers at $e^+e^-$ Colliders

past

<b>SPEAR</b>	MARK2	Drift Chamber
	MARK3	Drift Chamber
<b>DORIS</b>	PLUTO	MWPC
	ARGUS	Drift Chamber
<b>CESR</b>	CLEO1,2,3	Drift Chamber
<b>VEPP2/4M</b>	CMD-2	Drift Chamber
	KEDR	Drift Chamber
	NSD	Drift Chamber
<b>PETRA</b>	CELLO	MWPC + Drift Ch.
	JADE	Drift Chamber
	PLUTO	MWPC
	MARK-J	TEC + Drift Ch.
	TASSO	MWPC + Drift Ch.
<b>TRISTAN</b>	AMY	Drift Chamber
	VENUS	Drift Chamber
	TOPAZ	TPC

<b>PEP</b>	MARK2	Drift Chamber
	PEP-4	TPC
	MAC	Drift Chamber
	HRS	Drift Chamber
	DELCO	MWPC
<b>BEPC</b>	BES1,2	Drift Chamber
	ALEPH	TPC
<b>LEP</b>	DELPHI	TPC
	L3	Si + TEC
	OPAL	Drift Chamber
	MARK2	Drift Chamber
<b>SLC</b>	SLD	Drift Chamber
	KLOE	Drift Chamber
<b>DAPHNE</b>	BaBar	Drift Chamber
<b>KEKB</b>	Belle	Drift Chamber

present

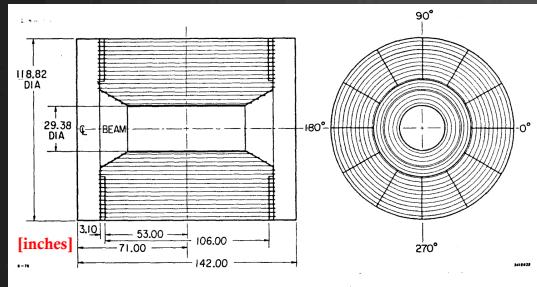
<b>VEPP2000</b>	CMD-3	Drift Chamber
<b>VEPP4</b>	KEDR	Drift Chamber
<b>BEPC2</b>	BES3	Drift Chamber
<b>S.KEKB</b>	Belle2	Drift Chamber

future

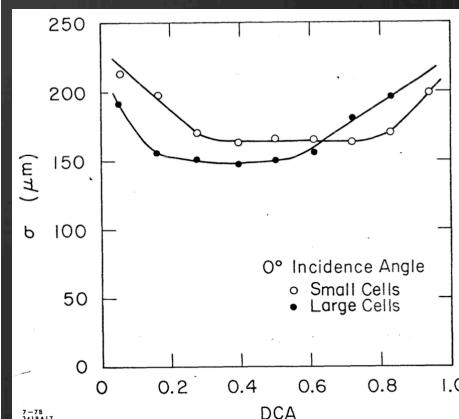
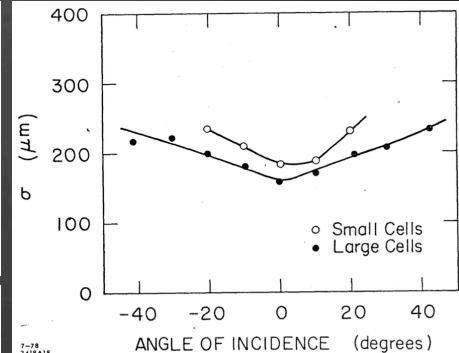
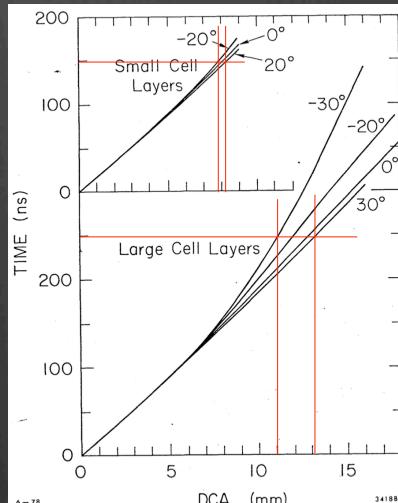
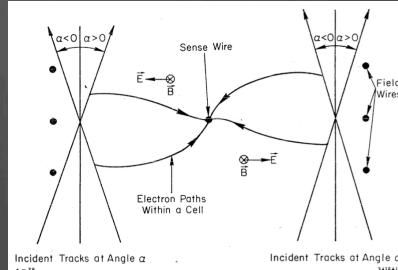
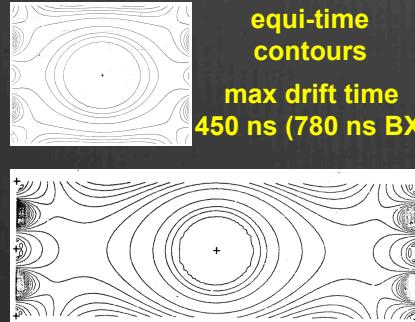
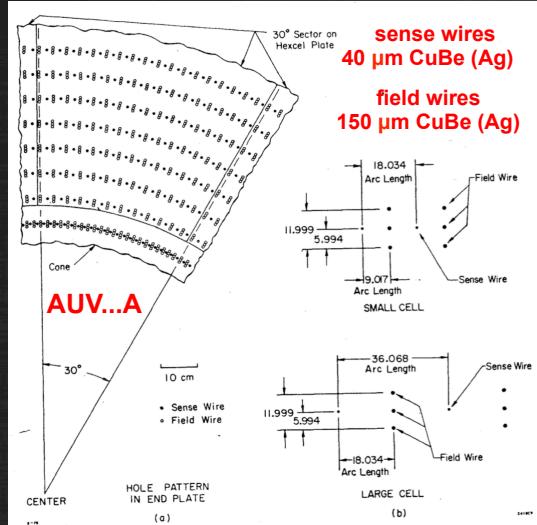
<b>ILC</b>	ILD	TPC
	SiD	Si
<b>CLIC</b>	CLIC	Si
<b>FCC-ee</b>	CLD	Si
	IDEA	Drift Chamber
<b>CEPC</b>	Baseline	TPC
	IDEA	Drift Chamber
<b>SCTF</b>	BINP	Drift Chamber
<b>STCF</b>	HIEPA	Drift Chamber

# MARK II at SPEAR (1978) where it all began ...

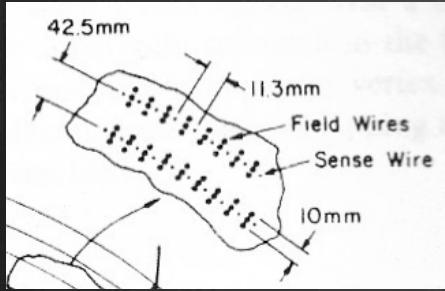
A Large Cylindrical Drift Chamber for the Mark II Detector at SPEAR - Davies-White, W.A. et al. Nucl.Instrum.Meth. 160 (1979) 227



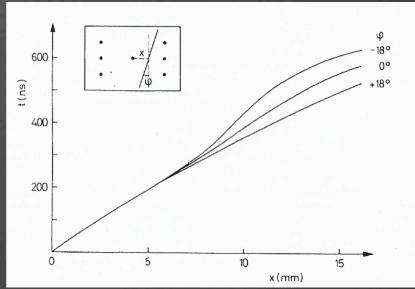
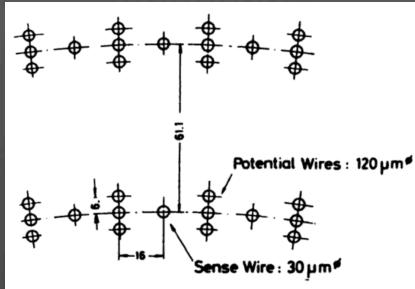
**Single sense wire cell**  
 ≈ 3 m diameter  
 ≈ 2.7 m active length  
 0.41 Tesla B-field  
 16 layers  
 6 axial + 10 stereo ( $\pm 3^\circ$ )  
 3204 drift cells (3:1)  
 22,000 wires  
 50% Ar – 50%  $C_2H_6$   
 2%  $X_0$  radial - 20%  $X_0$  e.p.  
 equi-time contours  
 max drift time  
 450 ns (780 ns BX)



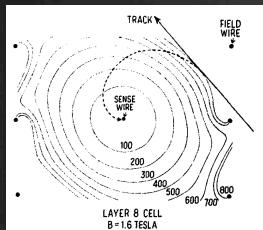
# Single sense wire "open" cells 3:1



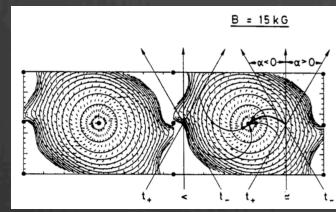
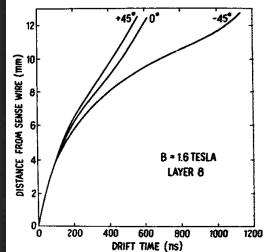
CLEO  
CESR  
1979



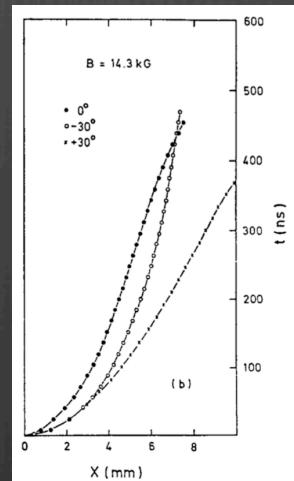
TASSO  
PETRA  
1979



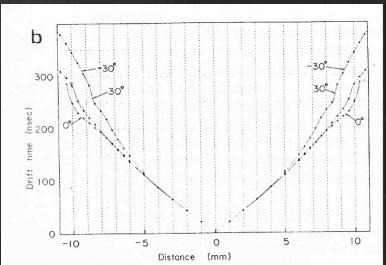
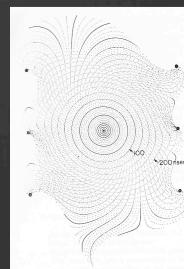
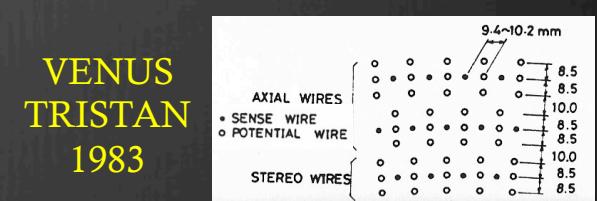
HRS  
PEP  
1980



CELLO  
PETRA  
1980



VENUS  
TRISTAN  
1983



# Single sense wire "open" cells 3:1

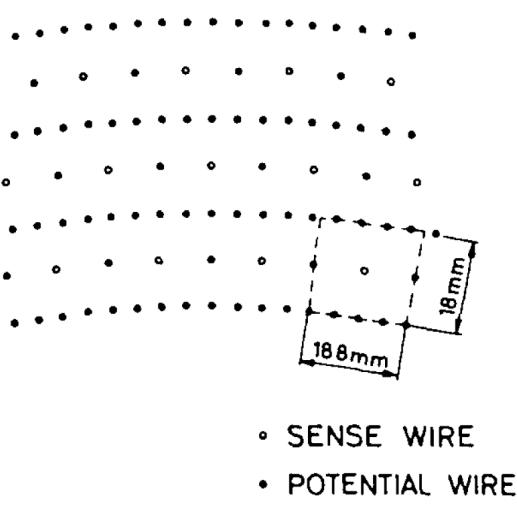
## Mechanics

	MARK II SPEAR (1978)	CLEO CESR (1979)	TASSO PETRA (1980)	CELLO PETRA (1980)	HRS PEP (1980)	VENUS TRISTAN (1985)
<b>Inner Radius [mm]</b>	370	172	320	170	152	250
<b>Outer Radius [mm]</b>	1450	950	1280	700	1100	1260
<b>Length [mm]</b>	2700	1930	3450	2200	2540	3000
<b>Axial layers</b>	6	9	9	7	7	20
<b>Stereo layers</b>	10	8	6	0	8	9
<b>Stereo angles [mrad]</b>	$\pm 52$	$\pm 52$	$\pm 70$	0	$\pm 60$	$\pm 60$
<b>Number of sense wires</b>	3204	5304	2340	1312	2448	7104
<b>Total number of wires</b>	13,000	22,000	9,000	5,200	10,000	28,000
<b>sense wires [<math>\mu\text{m}</math>]</b>	40 Cu-Be(Ag)	20 W(Au)	30 W(Au)	20 W(Au)	37 W(Au)	30 W-Re(Au)
<b>field wires [<math>\mu\text{m}</math>]</b>	150 Cu-Be(Ag)	115 Cu-Be(Ag)	120 Mo(Au)	50-100 Cu-Be	127 Cu-Be(Au)	125 Cu-Be(Au)
<b>Inner cylinder [mm/<math>X_0</math>]</b>	3.2 Lexan / 0.9%		5 fiberglass/ 3%		1 Be / 0.3%	1 C-f / 0.5%
<b>Outer cylinder [mm/<math>X_0</math>]</b>	6.25 Al / 7%		6.0 Al / 7%		0.6 Al / 0.7%	5 C-f / 2.4%
<b>End-plates [mm/<math>X_0</math>]</b>	6.35 Al (cone) 3.2 Al + ... / 20%		35 Al / 39%		9.5 Al (cone) 15.9 Al / 18%	21 Al / 24%

# Single sense wire "open" cells 3:1 Performance

	<b>MARK II SPEAR (1978)</b>	<b>CLEO CESR (1979)</b>	<b>TASSO PETRA (1980)</b>	<b>CELLO PETRA (1980)</b>	<b>HRS PEP (1980)</b>	<b>VENUS TRISTAN (1985)</b>
<b>B-field [T]</b>	0.4	1.0	0.5	1.3	1.6	0.75
<b>Cell Size [mm<sup>2</sup>]</b>	(9÷18)×12	11.3×10	16×12	15×18	17×10 ÷ 25×12	19×17
<b>Gas Mixture</b>	50 Ar / 50 C <sub>2</sub> H <sub>6</sub>	50 Ar / 50 C <sub>2</sub> H <sub>6</sub>	90 Ar / 10 CH <sub>4</sub>	90 Ar / 10 CH <sub>4</sub>	89 Ar / 10 CO <sub>2</sub> / 1 CH <sub>4</sub>	50 Ar / 50 C <sub>2</sub> H <sub>6</sub>
<b>Spatial Resolution [μm]</b>	150-200	250	220	170	200	150
<b>Momentum Resolution</b>	0.010p / 0.0145	0.012p / 0.007	0.020p / ?	0.029p / ?	0.005p / 0.003	0.0088p / 0.0012
<b>Δp [MeV/c] at 1 GeV/c</b>	17.6	13.9	>20.0	>30.0	5.8	14.9
<b>dE/dx</b>	//	6.5%	//	//	TOF + Cer.	//

# From "open" to "closed" cells



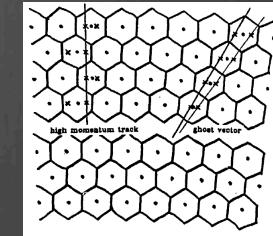
6:1  
ARGUS  
DORIS  
1982

A square-shape, closed cell implies more uniform and t-to-d relations less dependent from the track angle

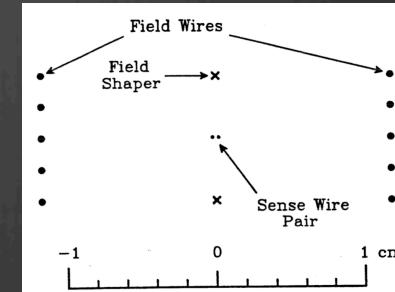
•	•	•	•	•	$V = 0$
$V_G$	$V_D$	$V_G$	$V_D$	$V_G$	
□	•	□	•	□	
X	•	X	•	X	
□	•	□	•	□	
•	•	•	•	•	$V = 0$

5(7):1  
DM2  
DCI  
1982

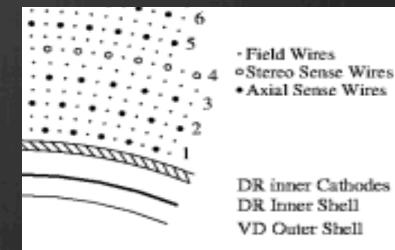
A larger ratio of field to sense wires allows for thinner field wires and, therefore, for less multiple scattering contribution from the wires to the momentum measurement.



2:1  
AMY  
TRISTAN  
1984



5:1  
MAC  
PEP  
1980



3:1  
CLEO2  
CESR  
1985

# Single sense wire "closed" cells

## Mechanics

	MAC PEP (1980)	ARGUS DORIS (1982)	DM2 DCI (1982)	AMY TRISTAN (1984)	CLEO2 CESR (1984)
<b>Inner Radius [mm]</b>	120	150	325	148	175
<b>Outer Radius [mm]</b>	455	860	871	655	945
<b>Length [mm]</b>	1890	2000	2400	1800	1890
<b>Axial layers</b>	4	18	5	25	40
<b>Stereo layers</b>	6	18	8	15	11
<b>Stereo angles [mrad]</b>	$\pm 50$	$\pm 40\text{--}80$	$\pm 52$	$\pm 79$	$\pm 52$
<b>Number of sense wires</b>	883	5940	2080	9048	12240
<b>Total number of wires</b>	6,500	31,000	17,000	32,000	49,000
<b>sense wires [<math>\mu\text{m}</math>]</b>	20 W(Au)	20 W-Re(Au)	20 W-Re(Au)	20 W(Au)	20 W(Au)
<b>field wires [<math>\mu\text{m}</math>]</b>	200 Cu-Be	120-200 Al(Au)	120-200 Al(Au)	160 Al(Au)	110 Al/Cu-Be(Au)
<b>Inner cylinder [mm/<math>X_0</math>]</b>	? / 1.6%	3.3 C-f / 1.5%			0.75 C-f+1 Al / 1.5%
<b>Outer cylinder [mm/<math>X_0</math>]</b>		6 Al / 6.7%			6.35 HC+1.6 Al / 3%
<b>End-plates [mm/<math>X_0</math>]</b>	19 SS / 110%	30 Al / 34%			31.7 Al / 36%

# Single sense wire "closed" cells

## Performance

	MAC PEP (1980)	ARGUS DORIS (1982)	DM2 DCI (1982)	AMY TRISTAN (1984)	CLEO2 CESR (1984)
<b>B-field [T]</b>	0.57	0.8	0.5	3.0	1.5
<b>Cell Size [mm<sup>2</sup>]</b>	(15÷23.5)×10	18×18.8	24×40	10×12	14×14
<b>Gas Mixture</b>	90 Ar / 10 CH <sub>4</sub>	97 C <sub>3</sub> H <sub>6</sub> / 3 C <sub>3</sub> H <sub>6</sub> O <sub>2</sub>	50 Ar / 50 C <sub>2</sub> H <sub>6</sub>	50 Ne / 50 C <sub>2</sub> H <sub>6</sub>	50 Ar / 50 C <sub>2</sub> H <sub>6</sub>
<b>Spatial Resolution [μm]</b>	180	150	180	200	180
<b>Momentum Resolution</b>	0.052p / ?	0.009p / 0.010	0.014p / 0.014	0.0070p / ?	0.0026p / 0.0057
<b>Δp [MeV/c] at 1 GeV/c</b>	>52	13.5	19.8	>10	6.3
<b>dE/dx</b>	//	5.0%	TOF + Cer.	//	6.0%

# Lesson #1 - from "open" to "closed" cell

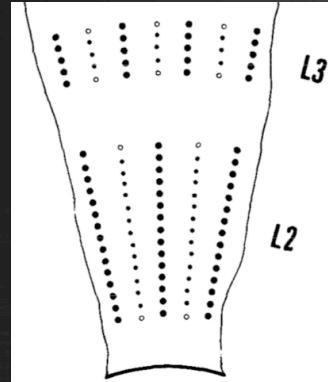
- closed cells limit the very long tails in the drift time distribution
- closed cells make the time-to-distance relations less dependent from the track angle
- square cells make the time-to-distance relations more isotropic
- small drift distance limits drift asymmetries due to Lorenz angle

... but

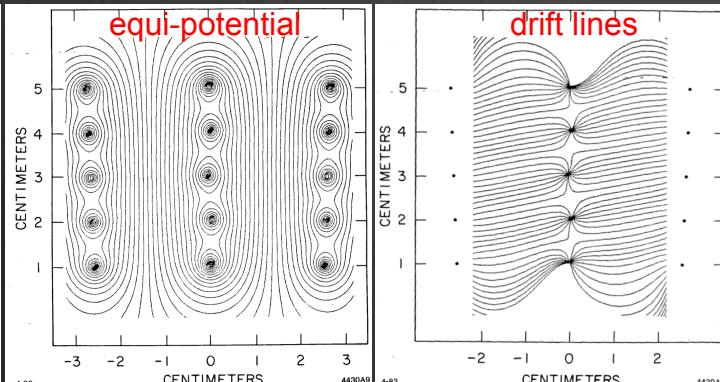
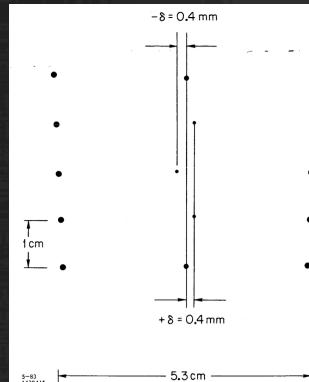
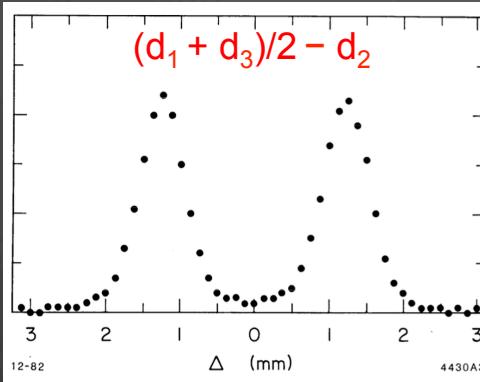
- portions of active volume not sampled between the cylindrical envelope of axial wires and the hyperboloid envelope of stereo wires
- small ratio of the number of field wires per sense wire (3:1) forces the use of thick field wires with consequences on multiple scattering contribution to momentum resolution and total load on end-plates
- some problems with left-right ambiguity and close tracks separation

# MARK3 at SPEAR – JADE at PETRA

F. Grancagnolo and A. Seiden, Large Drift Chambers with a Multi-Wire Cell Design, SCIPP 81/5



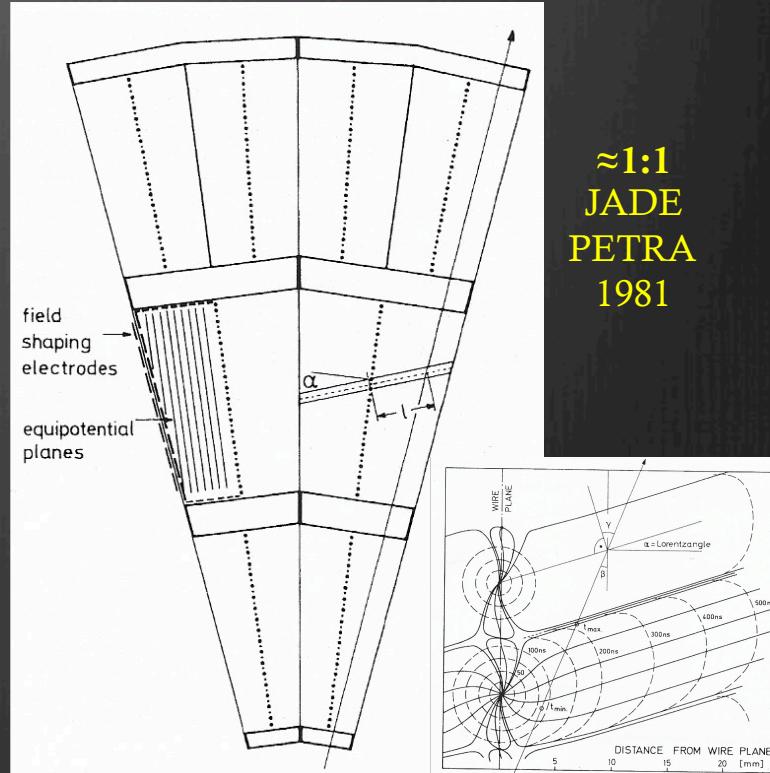
**2.33:1**  
MARK3  
SPEAR  
1980



F. Grancagnolo - DC at ee Colliders

12

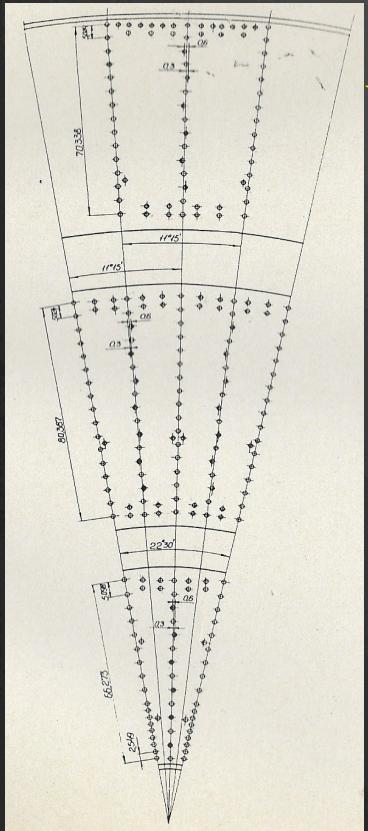
J. Heintze, Drift chambers and recent developments, NIM 156 (1978) 227



**≈1:1**  
JADE  
PETRA  
1981

Feb. 25, 2020

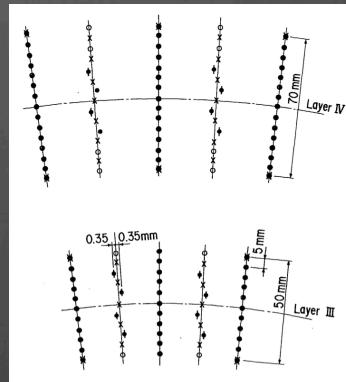
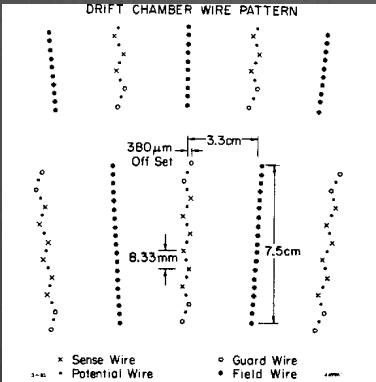
# Multi-wire and Jet-like cells



**6.8:1**  
CMD-2  
VEPP -2M  
1985

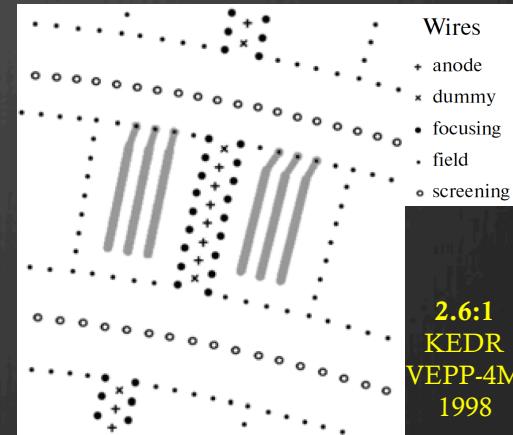
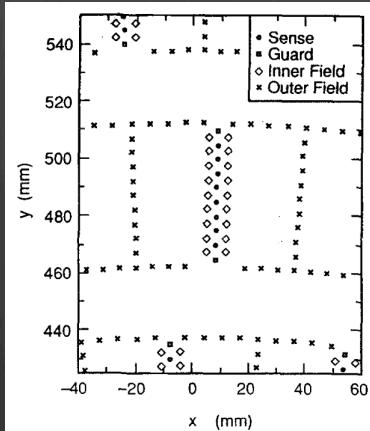
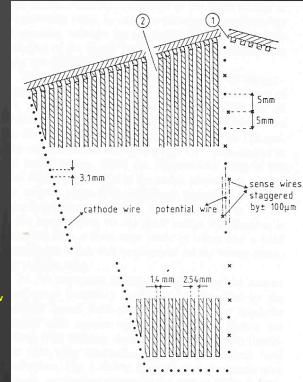
**5.3:1**  
MARK2  
PEP/SLC  
1985

**5.625:1**  
SLD  
SLC  
1988



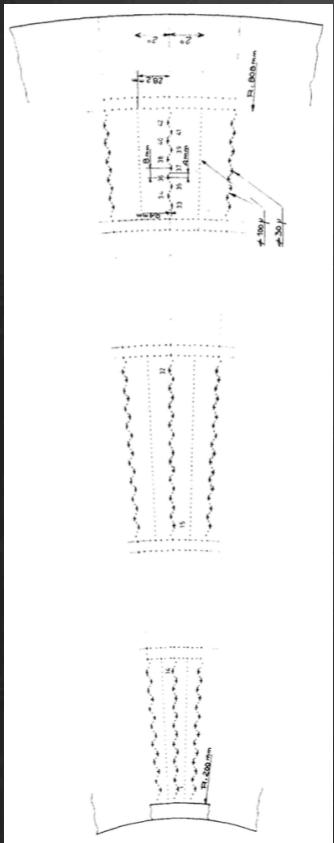
**6.5:1**  
BES  
BEPC  
1989

**4.3:1**  
OPAL  
LEP  
1988

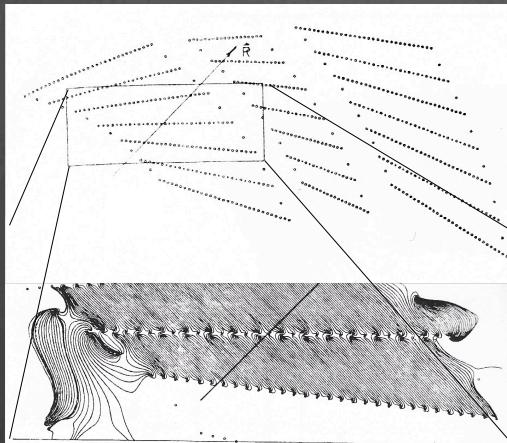


**2.6:1**  
KEDR  
VEPP-4M  
1998

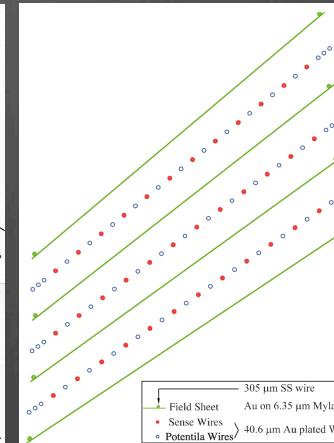
# More Jet-like cells



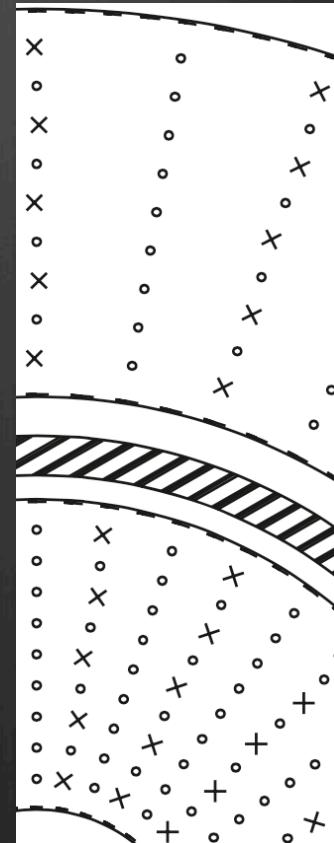
5.625:1  
AFS  
ISR  
1982



4.9:1  
CDF CTC  
Tevatron  
1988



4.25:1  
CDF COT  
Tevatron  
2002  
ZEUS  
HERA  
1992



2.6:1  
SND  
VEPP-2M  
1995

# Multi-wire and Jet-like cells

## Mechanics

	MARK3 SPEAR (1980)	JADE PETRA (1980)	CMD-2 VEPP-2M (1985)	MARK2 PEP/SLC (1985)	SLD SLC (1988)	OPAL LEP (1988)	BES/BESII BEPC (1989)	KEDR VEPP-4M (1998)
<b>Inner Radius [mm]</b>	140	180	25	192	200	245	155	125
<b>Outer Radius [mm]</b>	1140	800	295	1519	1000	1850	1150	535
<b>Length [mm]</b>	2337	2400	440	2300	2000	4000	2200	1100
<b>Axial layers</b>	12+4×3	16×2	6+7+6	6×6	4×8	159×1	5×4	4×6
<b>Stereo layers</b>	2×3	0	0	6×6	6×8	0	5×4	3×6
<b>Stereo angles [mrad]</b>	±150	0	0	±66	±41	0		±52
<b>Number of sense wires</b>	2000	1536	512	5832	5300	3816	2808	1512
<b>Total number of wires</b>	6,240	3360	3,500	37,000	35,000	20,000	19,400	16,000
<b>sense wires [<math>\mu\text{m}</math>]</b>	20 W(Au)/57 SS	25 W-Re(Au)	25 Ni-Cr	30 W(Au)	25 W(Au)	25 W-Re	30 W	28 W(Au)
<b>field wires [<math>\mu\text{m}</math>]</b>	175 Cu-Be	125-175 Cu-Be	10-20 Ti(Cu)	178-305 Cu-Be(Au)	150 Al(Au)	125-175 Cu-Be	100-178-200 Cu-Be	70-150 Ti(Au)
<b>Inner cylinder [mm/<math>X_0</math>]</b>	9.5 HC+mylar+Al / 0.2%			2.0 Be / 0.6%	Al + HC	1.5 C-f / 0.7%		1.5 C-f / 0.7%
<b>Outer cylinder [mm/<math>X_0</math>]</b>	6.25 Al / 7.0%			12.7 Al / 15.0%	Al + HC			5.0 G10 / 3.0%
<b>End-plates [mm/<math>X_0</math>]</b>	25.4 / 15% - 7.62 / 8.5%	25.4 G10 / 15.0%	10.0 G10 / 6.0%	51.0 Al / 57.0%	5.0 Al / 5.7%	32 G10 / 19.2% / 28 Al / 33.0%		20 G10 / 12.0%

# Multi-wire and Jet-like cells

## Performance

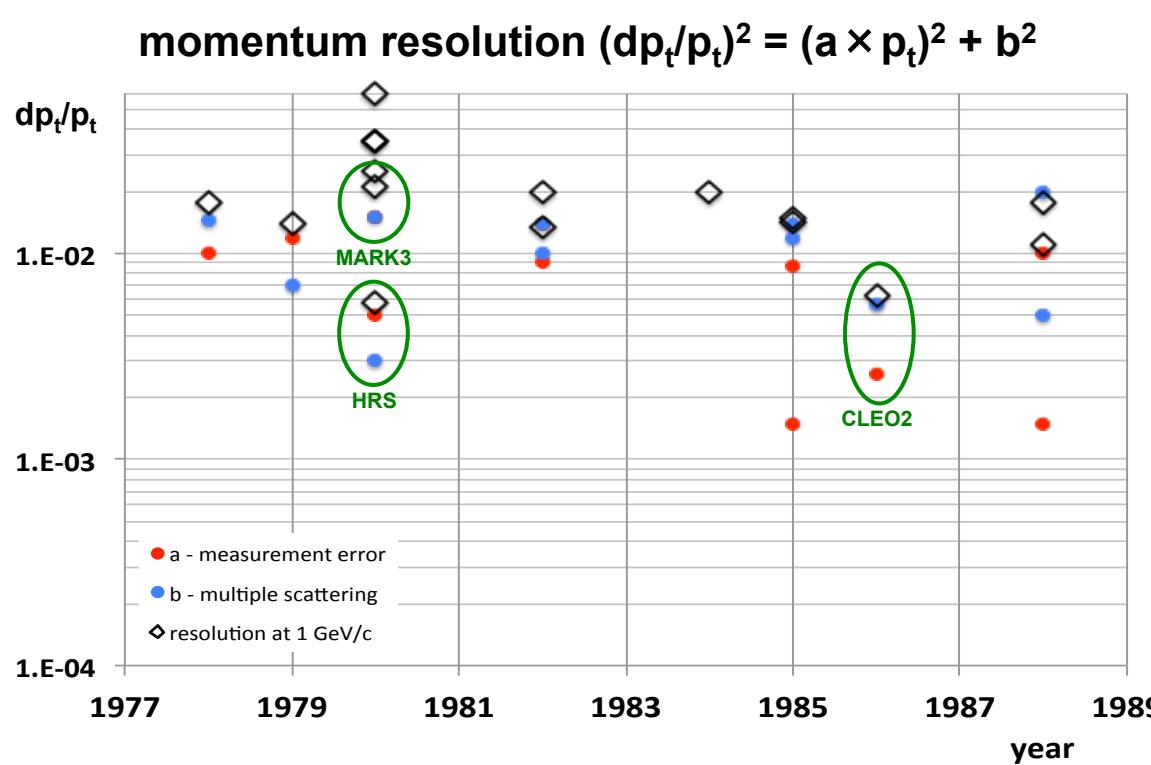
	MARK3 SPEAR (1980)	JADE PETRA (1980)	CMD-2 VEPP2M (1985)	MARK2 PEP/SLC (1985)	SLD SLC (1988)	OPAL LEP (1988)	BES/BESII BEPC (1989)	KEDR VEPP4M 1998)
<b>B-field [T]</b>	0.4	0.45	2.0	0.4	0.6	0.44	0.4	0.6 (1.8)
<b>Cell Size [mm<sup>2</sup>]</b>	(18÷30)×10	(10÷30)×10	(16÷28)×10	33×8.33	60×50	(30÷250)×10	30×10	30×4.5
<b>Gas Mixture</b>	HRS gas	88.7 Ar / 8.5 CH <sub>4</sub> / 2.8 iC <sub>4</sub> H <sub>10</sub>	80 Ar / 20 iC <sub>4</sub> H <sub>10</sub>	HRS gas	21 Ar / 72 CO <sub>2</sub> / 4 iC <sub>4</sub> H <sub>10</sub>	88 Ar / 10 CH <sub>4</sub> / 2 iC <sub>4</sub> H <sub>10</sub> at 4 bar	HRS gas	C <sub>2</sub> H <sub>2</sub> O (DME)
<b>Spatial Resolution [μm]</b>	220	135-165	95	175	155	135	240	115
<b>Momentum Resolution</b>	0.015p / 0.015	0.022p / ?	? / ?	0.0015p / 0.014	0.010p / 0.005	0.00150p / 0.02	0.018p / 0.018	0.02p / 0.03
<b>Δp [MeV/c] at 1 GeV/c</b>	21	>22	50	14.1	11.1	20	25	36
<b>dE/dx</b>	15.0%	6.0% - 8.5%	//	7.0%	6.4%	3.1% - 3.8%	8.5%	8.5%

# Lesson #2 - from single to multi-wire

- left-right ambiguity solved at the cell level
  - track finding facilitated by the definition of a point and a vector within a single cell
  - double track resolution improved with suitable front-end electronics
- ... but

- very long drift times
- portions of active volume not sampled between the cylindrical envelope of axial wires and the hyperboloid envelope of stereo wires
- need for extra (thick) wires to limit cross-talk between adjacent sense wires and for extra wires at cell boundary to limit long drifts
- only limited stereo angles allowed because of its radial dependence for long jet-like cells

# Momentum resolution in early chambers



$$(dp_t/p_t)^2 = [8\sqrt{5}\sigma_{r\phi}/(0.3BL^2\sqrt{N})]^2 p_t^2 + [5.4 \times 10^{-2}/BL\sqrt{(L/X_0)}]^2$$

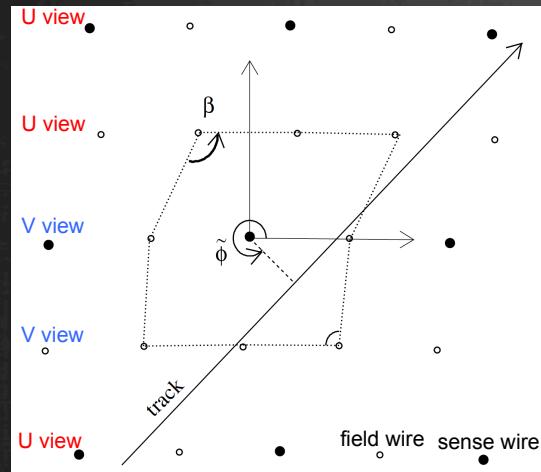
Despite the large variety of different parameters involved,  
**momentum resolution** (at  $p=1\text{GeV}/c$ ) clusters around **1-2%** for all chambers.

Initially, resolution dominated by the **sagitta measurement error**. With improved cell configurations, the dominant error became **multiple scattering**, claiming for a **breakthrough** in the **gas mixture** and in the **wires**.

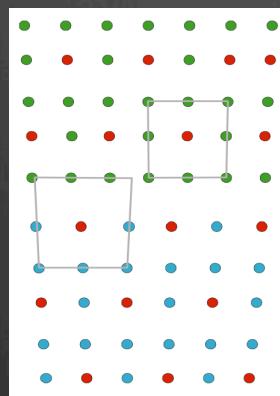
# Helium as Drift Chamber gas ...

- W. Zimmermann et al., *Helium-propane as drift chamber gas*, Nucl. Instrum. Meth. A243 (1986) 86
- F. Grancagnolo, *A Helium Drift Chamber as the Central Tracker of a B-Factory*, Proc. Workshop on Heavy Quarks Factory and Nuclear Physics Facility with Superconducting Linacs, Courmayeur, 1987, eds. E. De Sanctis, M. Greco, M. Piccolo and S. Tazzari (Atti di Coferenze, Società Italiana di Fisica, Bologna 1987) p. 599
- F. Grancagnolo, *A Central Tracking Detector for a B-Factory*, Nucl. Instrum. Meth. A277 (1989) 110

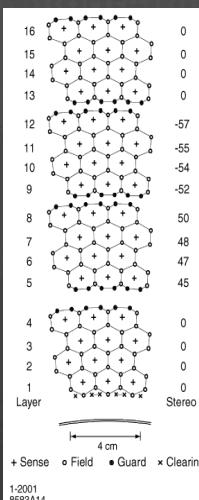
## ... and back to single sense wire cells



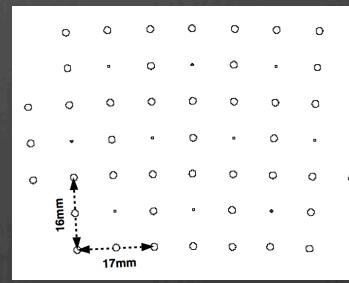
KLOE



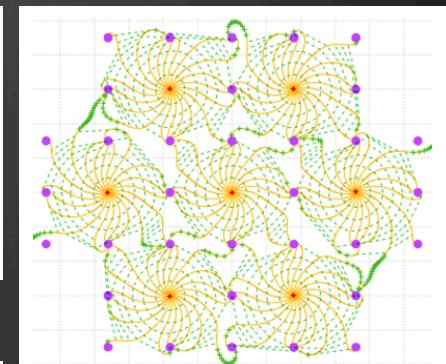
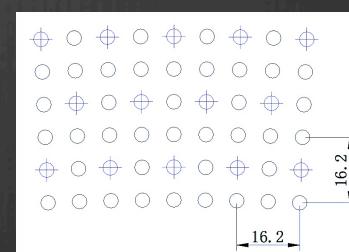
CLEO3



BABAR



BELLE



BELLE2

# Single wire cells – He gas Mechanics

	BESIII BEPC2 (2008)	KLOE DAPHNE (1998)	CLEO3 CESR2 (1998)	BABAR PEP2 (1998)	BELLE KEKB (1998)	BELLE2 KEKB (2017)
<b>Inner Radius [mm]</b>	63	250	125	236	77	160
<b>Outer Radius [mm]</b>	810	1980	820	808	880	1130
<b>Length [mm]</b>	2400	3300	2500	2800	2400	2420
<b>Axial layers</b>	5×4	0	8×2	4×4	6×5	5×6
<b>Stereo layers</b>	6×4	12+46	8×4	6×4	5×4	4×6
<b>Stereo angles [mrad]</b>	±35÷50	±60÷150	±20÷30		±42÷74	±60÷80
<b>Number of sense wires</b>	7000	12582	9796	7104	8400	14,336
<b>Total number of wires</b>	29,000	52,000	40,000	25,000	35,000	60,000
<b>sense wires [<math>\mu\text{m}</math>]</b>	25 W-Re(Au)	25 W(Au)	20 W-Re(Au)	20 W-Re(Au)	30W(Au)	30 W(Au)
<b>field wires [<math>\mu\text{m}</math>]</b>	110 Al(Au)	80 Al(Ag)	110 Al(Au)	80-120 Al(Au)	126 Al	126 Al
<b>Inner cylinder [mm/<math>X_0</math>]</b>	1.0 C-f / 0.45%	0.75 C-f + 0.2 Al / 0.55%	2.0 Roh + Al / 0.12%	1.0 Be / 0.28%	2.0 C-f / 1.1%	0.4 C-f / 0.22%
<b>Outer cylinder [mm/<math>X_0</math>]</b>	11.0 C-f / 5.0%	3.0 C-f + HC / 2.5%		C-f + HC / 1.5%	5.0 C-f / 2.6%	5.0 C-f / 2.6%
<b>End-plates [mm/<math>X_0</math>]</b>	25.0 Al / 28.0%	9.0 C-f / 4.7%	15.5 Al + ... / 17%	12/24 Al / 13.5%/27.0%	10.0 Al / 11.0%	10.0 Al / 11.0%

# Single wire cells – He gas Performance

	BESIII BEPC2 (2008)	KLOE DAPHNE (1998)	CLEO3 CESR2 (1998)	BABAR PEP2 (1998)	BELLE KEKB (1998)	BELLE2 KEKB (2017)
<b>B-field [T]</b>	1.0	0.6	1.5	1.5	1.5	1.5
<b>Cell Size [mm<sup>2</sup>]</b>	12×12 ÷ 16×16	20×21 + 30×31.5	14×14	12×18	8×15.5 + 10×17	87.5 + 15,25
<b>Gas Mixture</b>	60 He / 40 C <sub>2</sub> H <sub>6</sub>	90 He / 10 iC <sub>4</sub> H <sub>10</sub>	60 He / 40 C <sub>2</sub> H <sub>6</sub>	80 He / 20 iC <sub>4</sub> H <sub>10</sub>	50 He / 50 C <sub>2</sub> H <sub>6</sub>	50 He / 50 C <sub>2</sub> H <sub>6</sub>
<b>Spatial Resolution [μm]</b>	120	200	110	125	130	130
<b>Momentum Resolution</b>	0.0032p / 0.0037	0.0005 / 0.0026	0.0016p / 0.0028	0.0015p / 0.0045	0.0019p / 0.0030	0.0011p / 0.0025
<b>Δp [MeV/c] at 1 GeV/c</b>	4.9	2.6	3.2	4.7	3.5	2.7
<b>dE/dx</b>	6%-7%	4.6%	5.0%	7.5%	6.9%	6.9%

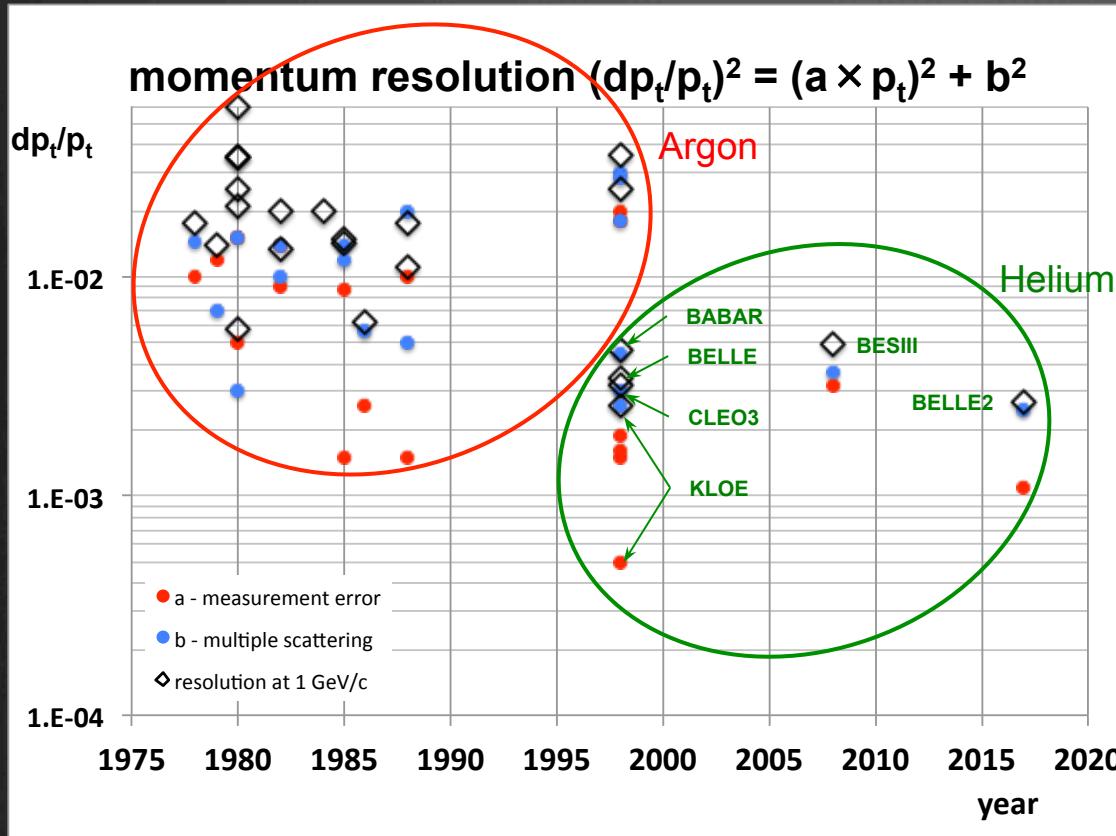
# Lesson #3 – small cells and He gas

- He radiation length 50× longer than Ar
- slower drift velocity implies smaller Lorenz angle for a given B-field
- He has a smaller cross section for low energy photons than Ar
- small size cells limit the electron diffusion contribution to spatial resolution
- small size cells provide high granularity (improving occupancy) and allow for a larger number of hits per track, improving spatial resolution

... but

- portions of active volume not sampled between the cylindrical envelope of axial wires and the hyperboloid envelope of stereo wires
- accumulation of trapped electrons and ions in a region of very low field
- longitudinal gain variation at boundaries between axial and stereo layers
- spatial resolution dominated by ionization statistics for short drift distances
- adding more quencher to compensate, mitigates the advantage of He

# Momentum resolution after Helium



$$(dp_t/p_t)^2 = [8\sqrt{5}\sigma_{r\phi}/(0.3BL^2\sqrt{N})]^2 p_t^2 + [5.4 \times 10^{-2}/BL\sqrt{(L/X_0)}]^2$$

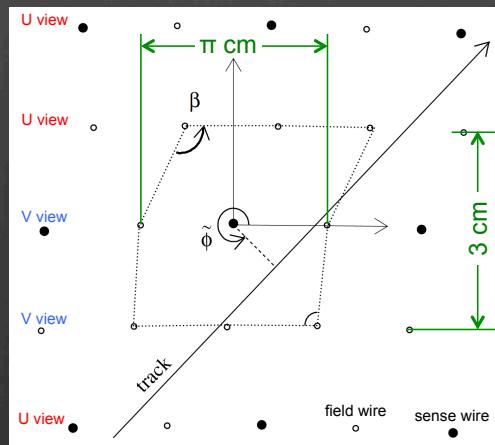
Momentum resolution  
 $\leq$  a few  $\times 10^{-3}$

However,  
too large amounts of  
quencher mitigate  
the advantages of the  
long radiation length  
of Helium

# "Full" stereo configuration: KLOE

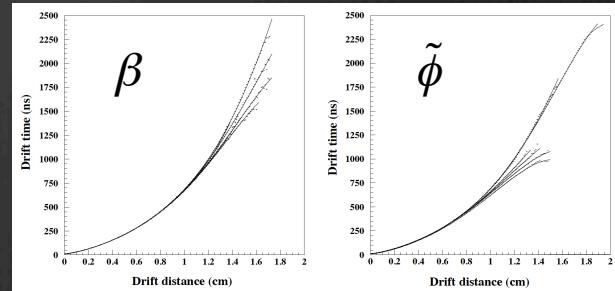
A configuration with only perfectly nested alternating sign stereo layers (no axial layer) fills the gaps occurring in a mixed stereo-axial configuration, rendering the the chamber more isotropic and fully sampled, thus increasing the number of hits on a track for a given cell size.

In **KLOE**, this is achieved by having the field wires layer of the cell outer bound at a stereo angle of opposite sign w.r.t. the sense wire layer and to the field wires layer of the cell inner bound



The stereo configuration is obtained with constant stereo drop at the middle transverse plane. This, however, besides causing a small longitudinal variation of the cell aspect ratio, implies:

**time to distance relations which depend on the track angle and on the cell periodicity in z.**



# Lesson #4 – full stereo configuration

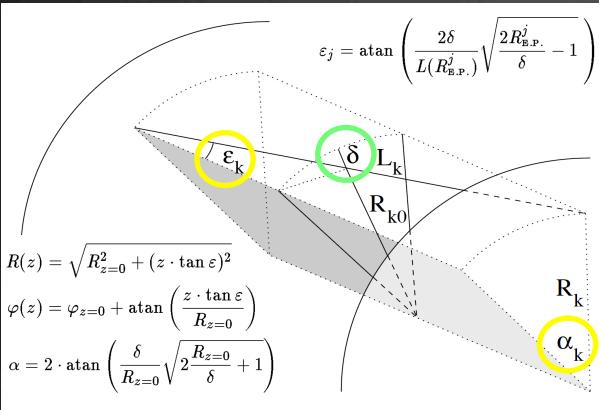
- no gaps between axial and stereo layers which may trap ions and electrons in regions of very low electric field
- constant sense wire gain as a function of the longitudinal coordinate
- larger number of hits on a track for a given cell size
- maximizes the number of measurements of the longitudinal coordinate
- two stereo views enable 3D reconstruction in a natural way

... but

- open top cells cause a dependence of the time-to-distance relations from the track angle and from the cell longitudinal periodicity
- constant stereo drop (as in KLOE) changes the cell aspect ratio along z (radial cell size constant but azimuthal width increased at end-plates)
- constant stereo angle generates cell distortions for large stereo angles

# MEG2 approach at "full" stereo

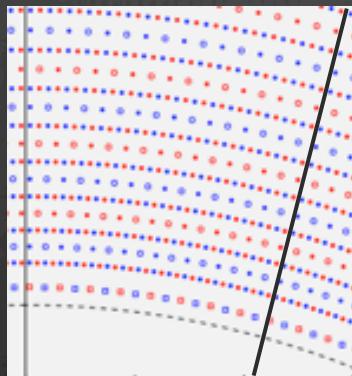
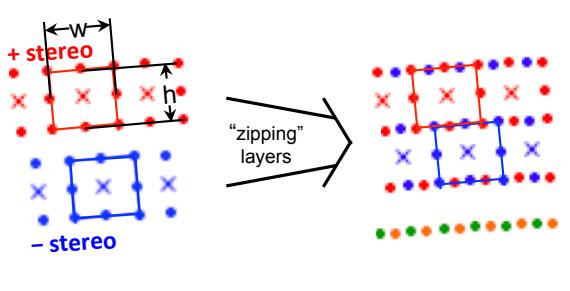
see Tassielli, next talk



**Constant transverse stereo angle projection  $\alpha_k$  preserves the cell aspect ratio:**

**"square" cells by construction:  $w_k = h_k$  remain such at any  $z$  [ $w_k(z=\pm L/2) = h_k(z=\pm L/2) = 1.035 w_k(z=0) = 1.035 h_k(z=0)$  for 100 mrad stereo angle and 2 m wire length]**  
**no  $\beta$  angle dependence - no  $\Phi$  angle dependence in principle, one single t-to-d scalable for all layers**

## Layer assembly



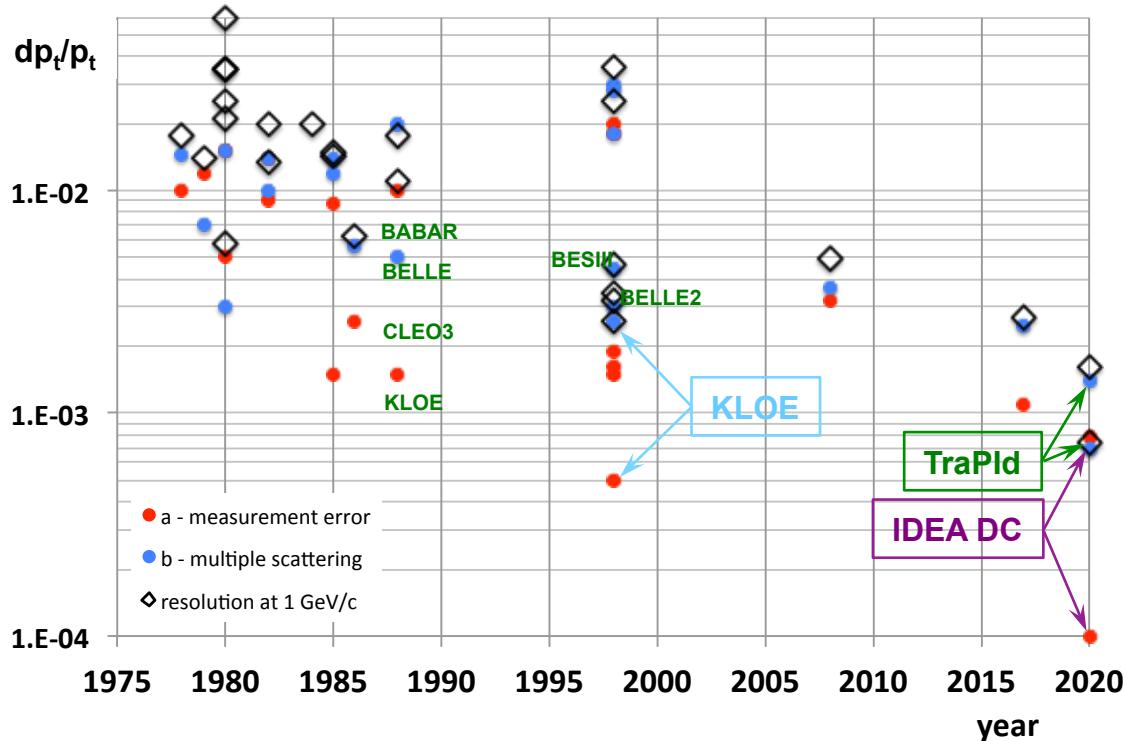
This configuration requires more **field wires per sense wire** (5:1, as opposed to 3:1 in KLOE) allowing for **thinner field wires**, therefore, even **less m.s. contribution and less load on the end plates**.

# Lesson #5 – summary

- the configuration offering the best performance in terms of **momentum resolution** is one with small, single sense wire closed **cells**, arranged in contiguous layers of opposite sign stereo angles, obtained with **constant stereo angle transverse projection**
- the gas mixture is based on helium with a small amount of quencher (90% He / 10%  $i\text{C}_4\text{H}_{10}$ , KLOE gas) which, besides low multiple scattering contribution, allows for the exploitation of the **cluster timing** technique, for improved spatial resolution, and of the **cluster counting** technique, for excellent particle identification
- suggested wire material is **Ag coated Al**, but lighter materials are under scrutiny (like **metal coated carbon monofilaments**)

# IDEA DC and TraPId $p_t$ resolution

$$\text{momentum resolution } (dp_t/p_t)^2 = (a \times p_t)^2 + b^2$$



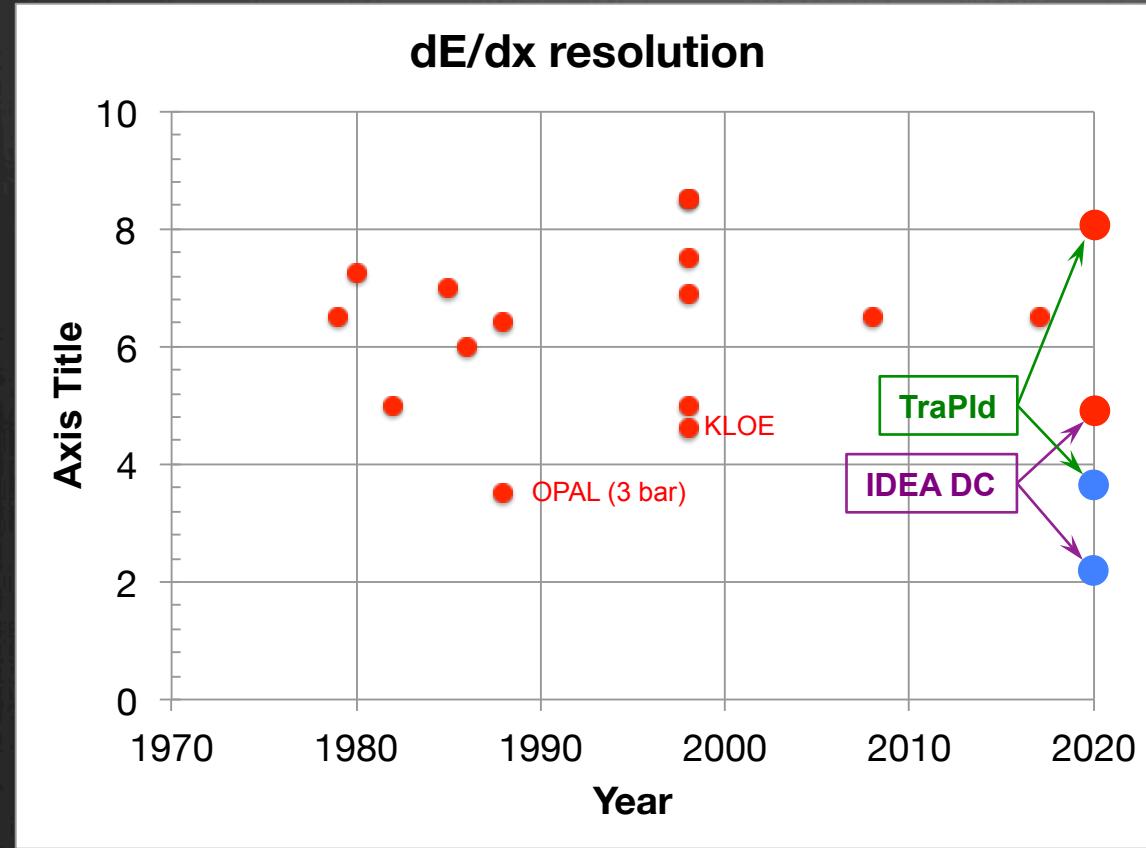
## IDEA DC

proposed for the IDEA  
detector  
at FCC-ee and CEPC

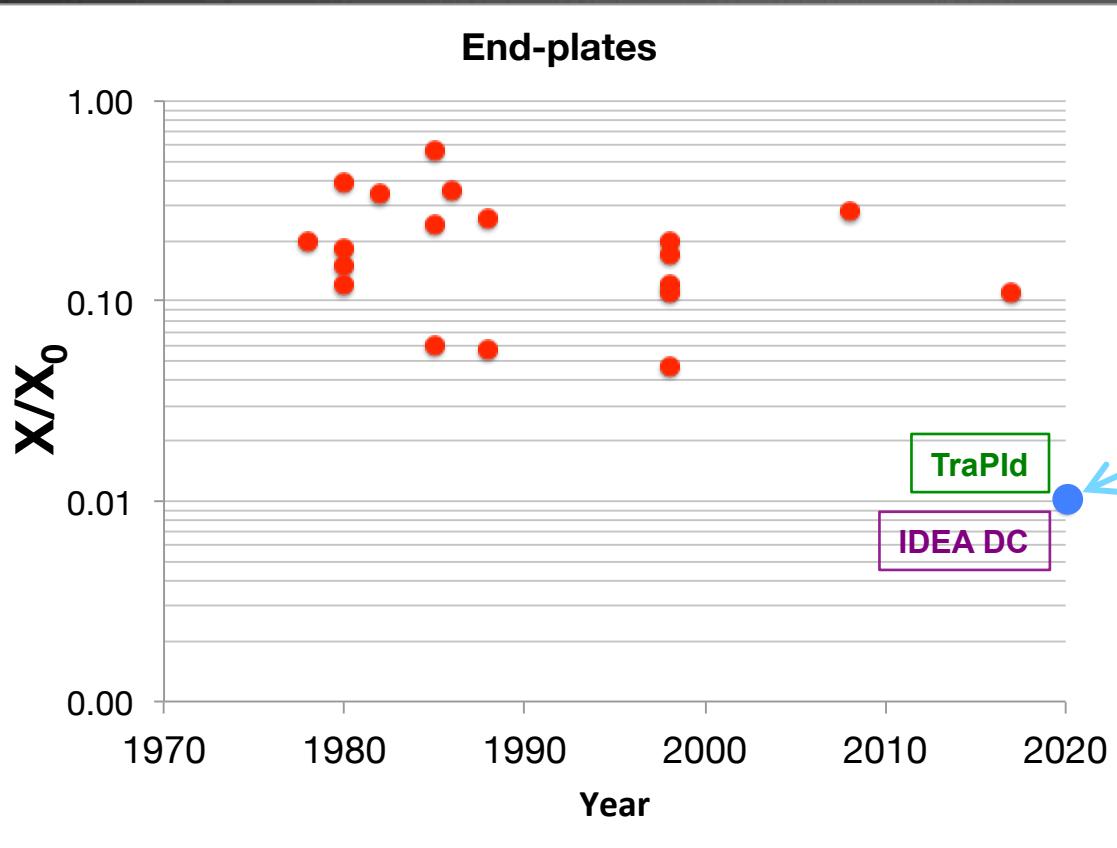
## TraPId

TRAcking and  
Particle Identification  
Drift Chamber for  
SCTF at BINP

# IDEA DC and TraPlId $dE/dx$ resolution



# IDEA and TraPlid end-plate $X_0$



please,  
have a look at **Poster #91**  
"New Concepts for Light  
Mechanical Structures of  
Cylindrical Drift Chambers"

# Conclusions

- we have presented the evolution of **momentum resolution** for drift chambers at  $e^+e^-$  colliders over the past 40 years
- we have briefly summarized the **particle identification** capabilities with  **$dE/dx$**  and the potentialities with cluster counting ( **$dN/dx$** )
- we have briefly listed the impact of the drift chambers **mechanical structure** as passive material in front of the electromagnetic end-caps calorimeters and the relative improvements over the years
- we have **not** discussed about the **front-end electronics** evolution and the different techniques of **data acquisition and processing** of the wire signals.

# Momentum and Angular Resolutions

<https://doi.org/10.1016/j.nima.2018.08.078>

An extension of the Gluckstern formulae for multiple scattering: Analytic expressions for track parameter resolution using optimum weights



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## ARTICLE INFO

Keywords:  
Tracking  
Multiple scattering  
Impact parameter resolution  
Momentum resolution

## ABSTRACT

Momentum, track angle and impact parameter resolution are key performance parameters that tracking detectors are optimised for. This report presents analytic expressions for the resolution of these parameters for equal and equidistant tracking layers. The expressions for the contribution from position resolution are based on the Gluckstern formulae and are well established. The expressions for the contribution from multiple scattering using optimum weights are discussed in detail.

$$\begin{aligned} \frac{\Delta p_T}{p_T}|_{res.} &= \frac{\sigma_{r\phi} p_T}{0.3 B_0 L_0^2} \sqrt{\frac{720N^3}{(N-1)(N+1)(N+2)(N+3)}} \\ &\approx \frac{12 \sigma_{r\phi} p_T}{0.3 B_0 L_0^2} \sqrt{\frac{5}{N+5}} \\ \frac{\Delta p_T}{p_T}|_{m.s.} &= \frac{N}{\sqrt{(N+1)(N-1)}} \frac{0.0136 \text{ GeV/c}}{0.3 \beta B_0 L_0} \\ &\times \sqrt{\frac{d_{tot}}{X_0 \sin \theta}} \left( 1 + 0.038 \ln \frac{d}{X_0 \sin \theta} \right) \\ &\approx \frac{0.0136 \text{ GeV/c}}{0.3 \beta B_0 L_0} \sqrt{\frac{d_{tot}}{X_0 \sin \theta}} \end{aligned}$$

$$\begin{aligned} \Delta d_0|_{res.} &= \frac{3\sigma_{r\phi}}{\sqrt{(N-1)(N+1)(N+2)(N+3)}} \times \\ &\sqrt{\left(N^2 - \frac{N}{3} - \frac{2}{3}\right) + \frac{4(7N^3 - N^2 - N)r_0}{L_0} + \frac{4(7N^3 - N^2 - N)r_0^2}{L_0^2} + \frac{40N^3r_0^3}{L_0^3} + \frac{20N^3r_0^4}{L_0^4}} \\ &\approx \frac{3\sigma_{r\phi}}{\sqrt{N+5}} \sqrt{1 + \frac{8r_0}{L_0} + \frac{28r_0^2}{L_0^2} + \frac{40r_0^3}{L_0^3} + \frac{20r_0^4}{L_0^4}} \\ \Delta d_0|_{m.s.} &= \frac{r_0}{\beta p_T} f\left(\frac{d}{X_0 \sin \theta}\right) \sqrt{\frac{N-3/4}{N-1} + \frac{N}{2(N-1)} \left(\frac{r_0}{L_0}\right)^2 + \frac{N^2}{4(N-1)} \left(\frac{r_0}{L_0}\right)^2} \\ \Delta d_0|_{m.s.}^{opt} &= \frac{r_0}{\beta p_T} f\left(\frac{d}{X_0 \sin \theta}\right) \sqrt{1 + \left(\frac{r_0}{L_0}\right)^2} \\ &\approx \frac{0.0136 \text{ GeV/c}}{\beta p_T} r_0 \sqrt{\frac{d}{X_0 \sin \theta}} \sqrt{1 + \left(\frac{r_0}{L_0}\right)^2} \\ \Delta z_0|_{res.} &= \frac{2\sigma_z}{\sqrt{(N+1)(N+2)}} \sqrt{\left(N + \frac{1}{2}\right) + \frac{3Nr_0}{L_0} + \frac{3Nr_0^2}{L_0^2}} \\ &\approx \frac{2\sigma_z}{\sqrt{N+3}} \sqrt{1 + \frac{3r_0}{L_0} + \frac{3r_0^2}{L_0^2}} \\ \Delta z_0|_{m.s.} &= \frac{r_0}{\sin \theta \beta p_T} f\left(\frac{d}{X_0 \sin \theta}\right) \\ &\approx \frac{0.0136 \text{ GeV/c}}{\beta p_T} \frac{r_0}{\sin \theta} \sqrt{\frac{d}{X_0 \sin \theta}} \end{aligned}$$

$$\begin{aligned} \Delta \theta|_{res.} &= \frac{\sigma_z \sin^2 \theta}{L_0} \sqrt{\frac{12N}{(N+1)(N+2)}} \\ &\approx \frac{2 \sigma_z \sin^2 \theta}{L_0} \sqrt{\frac{3}{N+3}} \\ \Delta \theta|_{m.s.} &= \frac{\sin \theta}{\beta p_T} f\left(\frac{d}{X_0 \sin \theta}\right) \\ &\approx \frac{0.0136 \text{ GeV/c} \sin \theta}{\beta p_T} \sqrt{\frac{d}{X_0 \sin \theta}} \end{aligned}$$

$$\begin{aligned} \Delta \phi|_{res.} &= \frac{\sqrt{12}\sigma_{r\phi}}{L_0 \sqrt{(N-1)(N+1)(N+2)(N+3)}} \\ &\times \sqrt{(16N^3 + 2N^2 - 3N) + \frac{60N^3 r_0}{L_0} + \frac{60N^3 r_0^2}{L_0^2}} \\ &\approx \frac{\sigma_{r\phi}}{L_0} \frac{8\sqrt{3}}{\sqrt{N+5}} \sqrt{1 + \frac{15}{4} \frac{r_0}{L_0} + \frac{15}{4} \frac{r_0^2}{L_0^2}} \\ \Delta \phi|_{m.s.} &= \frac{1}{\beta p_T} f\left(\frac{d}{X_0 \sin \theta}\right) \\ &\times \sqrt{\frac{N-3/4}{N-1} + \frac{N}{N-1} \left(\frac{r_0}{L_0}\right)^2 + \frac{N^2}{N-1} \left(\frac{r_0}{L_0}\right)^2} \\ \Delta \phi|_{m.s.}^{opt} &= \frac{1}{\beta p_T} f\left(\frac{d}{X_0 \sin \theta}\right) \\ &\times \sqrt{1 + 2 \left(\frac{r_0}{L_0}\right)^2 + 4 \left(\frac{r_0}{L_0}\right)^2} \quad N_{opt} = 2 + \frac{1}{2} \frac{L_0}{r_0} \\ &\approx \frac{0.0136 \text{ GeV/c}}{\beta p_T} \sqrt{\frac{d}{X_0 \sin \theta}} \sqrt{1 + 2 \left(\frac{r_0}{L_0}\right)^2 + 4 \left(\frac{r_0}{L_0}\right)^2} \end{aligned}$$

# $dE/dx$ and $dN_{cl}/dx$ Resolutions

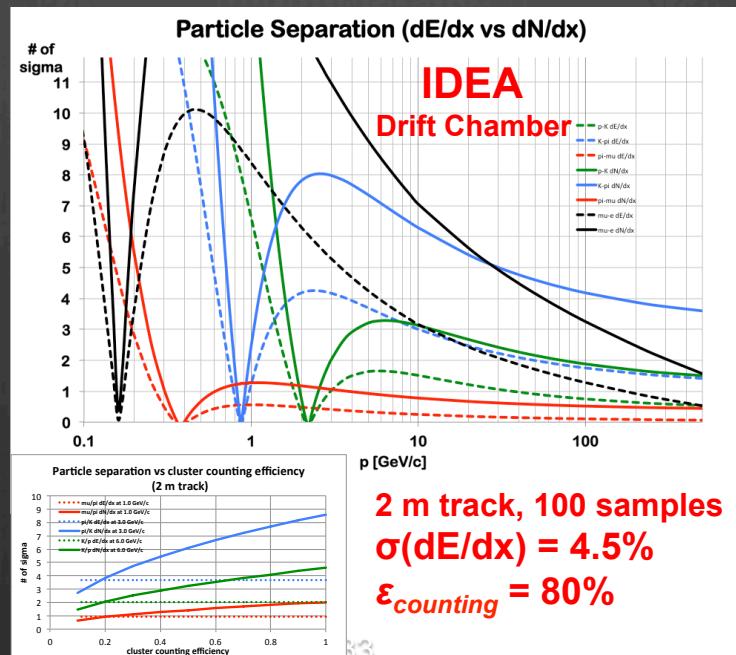
$$\frac{\sigma_{dE/dx}}{(dE/dx)} = 0.41 \cdot n^{-0.43} \cdot (L_{track} [m] \cdot P[atm])^{-0.32}$$

A. H. Walenta et al., *Measurement of the ionization loss in the region of relativistic rise for noble and molecular gases*, Nucl. Instr. and Meth. 161 (1979) 45-58.

- ❖ 5-80% truncated mean method
- ❖ statistical fluctuations of gas gain (< 1%)
  - drift distance dependence
  - z-dependence along the wire
  - wire sagging ( $\Delta w/w < 3 \times 10^{-3}$ )
- ❖ statistical fluctuation of energy loss (Landau)
- ❖ attachment (gas quality)
- ❖ avalanche saturation (angle dependence)
- ❖ rate effects
- ❖ double track separation
- ❖ wire to wire calibration

$$\frac{\sigma_{dN_{cl}/dx}}{(dN_{cl}/dx)} = (\varepsilon_{counting} \cdot \delta_{cluster} \cdot L_{track})^{-0.5}$$

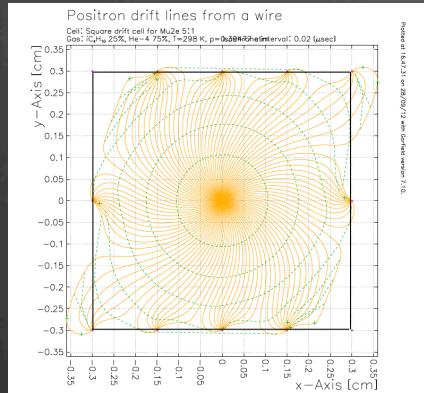
G. Cataldi, F. Grancagnolo and S. Spagnolo, *Cluster counting in helium based gas mixtures*, Nucl. Instr. and Meth. A386 (1997) 458-469.



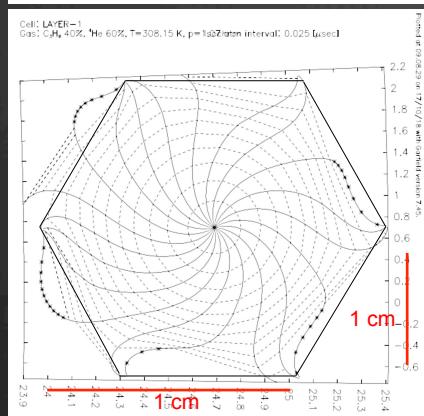
- ❖ Poisson statistics
- ❖  $\delta_{cluster} = 12.5$  cluster/cm in (90%He-10% $C_4H_{10}$ )
- ❖ outperforms  $dE/dx$  by a factor  $\times 2$
- ❖ even at very low counting efficiency ( $\varepsilon_{counting} \approx 20\%$ ) better than  $dE/dx$
- ❖ insensitive to
  - gas gain variations
  - lower dependence on gas composition
  - slighter dependence on avalanche saturation
- ❖ no wire to wire calibration needed

# Square versus Hexagonal cells

$B = 1 \text{ T}$   
75%He-25% $\text{iC}_4\text{H}_{10}$



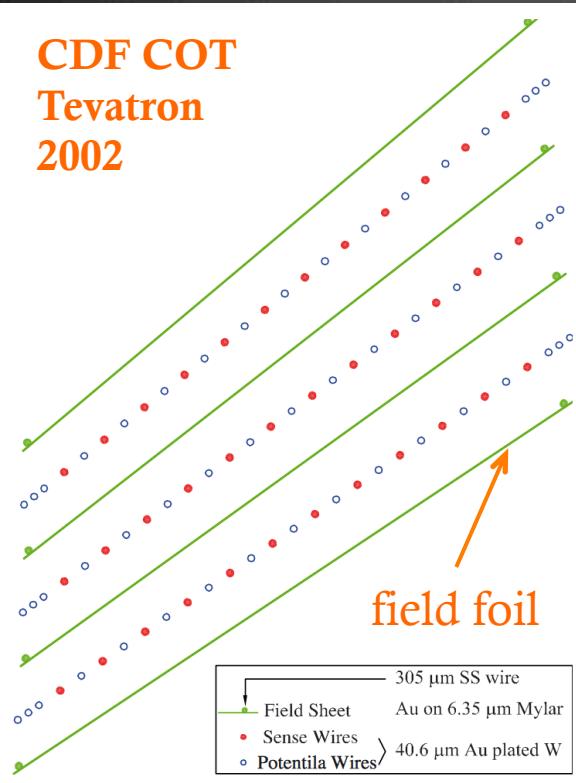
$B = 1.5 \text{ T}$   
60%He-40% $\text{C}_3\text{H}_8$



- small deviation of equi-time from perfect polygonal shape: 3.3% vs. 3.1%
- field to sense wire ratio: 5 to 1 vs. 2 to 1 for equal gain
  - more field wires implies more isotropic E-field and smaller distortions due to the  $E \times B$  effects
  - thinner field wires: 40  $\mu\text{m}$  vs. 100-125  $\mu\text{m}$
  - less multiple scattering
  - less load on end plates
- smaller gaps in B-field
- larger time-to-distance distortions
  - longer tails ( $> 500 \text{ ns}$  for 1 cm cell) in signal pulse (hit pattern,  $dE/dx$ , pile up)
- easier implementation of a full stereo configuration

# field foil versus field wires

CDF COT  
Tevatron  
2002



- very effective solution to confine broken wires within a limited region
- very uniform field at the cell boundary
- larger cathode surface allows for running at higher gain
- no such a radial symmetry with single sense wire cells
- azimuthal symmetry for axial wire layers but not for stereo layers
- Moreover:
  - 6.35  $\mu\text{m}$  Mylar + 2 $\times$ 0.035  $\mu\text{m}$  Au  =  $2.4 \times 10^{-4} X_0$
  - 40  $\mu\text{m}$  diameter Au plated Al (4/cm)  =  $1.0 \times 10^{-5} X_0$
- Load on end plates: 560 g/cm of foil, 80 g for 4 wires/cm