# Stress simulation on a round wheel W target 

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## Outline

- Introduction
- Simulation results of full ring and sliced ring
- Summary


## Introduction

- Main structure of the model

- For model 1, there is no slots in tungsten part;
- For model 2, the tungsten is sliced to 10 parts by the slot with a width of 0.2 mm ;
- An intermetallic contact between the W and the Cu, like brazing, is assumed, with a thermal conductance of $2 \mathrm{~W} /\left(\mathrm{cm}^{\wedge} 2-\mathrm{K}\right)$
- The average power is deposited uniformly in time and space over the top part of the W. In total about 35 Kw
- The water temperature is 50 K .

Model-1

## Model-1



## - Boundaries:

- Water Temperature: 50C
- Thermal Conductance for both of water- Cu and $\mathrm{W}-\mathrm{Cu}$ surface: $0.02 \mathrm{~W} / \mathrm{mm}^{\wedge} 2$
- Power is only deposited in the top part of the W with $0.0795 \mathrm{~W} / \mathrm{mm}^{\wedge} 3$
- There is a Cu bar with diameter of 30 mm in the center. We fixed it.



## Results: Temperature distribution



## ANSYS



## Temperature



There will be a temperature jump at the interface.


## Temperature




The temperature is obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Results: v. M. Stresses



## v. M. stresses


interface


## The v. M. stresses




The $\mathrm{v} . \mathrm{M}$. stresses are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Sigma r




The stresses at radial direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Sigma phi




The stresses at phi direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Sigma z




The stresses at axial direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## H: Copy of Static Structural <br> Equivalent Stress

Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1
Custom
Max: 258.9
Min: 10.625
2017/3/29 17:32
129.58
$\square 129.58$ $-103.63$ $-90.659$ 77.684 64.71 54.71
51.736 51.736
38.761 38.761
25.787
12.812

ANSYS


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Equivalent Stress
Type: Equivalent (von-Mises) Stress
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Time: 1
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Custom
Max: 258.9
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- 129.58
$\square \begin{aligned} & 129.58 \\ & 116.61\end{aligned}$
$-103.63$
$-90.659$
77.684
$-64.71$
51.736
38.761
38.761
25.787
12.812

ANSYS
R17.0



Stresses at the other side of Cu .

Stresses for Cu at interface.

The Stress here should be because the center bar is fixed as a boundary condition.

## Model-2:

## Sliced W-target with 10 gaps of $\mathbf{0 . 2 m m}$

## Model-2: sliced W-target with 10 gaps of 0.2 mm




## Results: Temperature distribution

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They are essentially the same as in the full ring, as expected.

## Results: Stresses


$\because$

## v. M. Stresses distribution at interface


v. M. stress in-plane of contact surface at $W$ wheel

v. M. stress in-plane of contact surface at Cu wheel

## Stresses at center of the sector



The v. M. stresses



- The v. M. stresses are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .
- There a binning problem. It should not be a real data.


## Sigma r




The stresses at radial direction (sigma $x$ ) are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Sigma phi




The stresses at phi direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Sigma z




The stresses at axial direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Stresses at end of the sector



## The v. M. stresses




- The v. M. stresses are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .
- Path for $W$ is on the surface of $W$ due to the gaps.
- Discussion: the max. stress in this picture appearing at the point shown in the picture is about 164 Mpa . However, the max. stress for whole model is about 208MPa. It appears at the similar point in one of connection positions between gaps and Cu cooler.


## Sigma r




The stresses at radial direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W.

## Sigma phi




The stresses at phi direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W.

## Sigma z




The stresses at axial direction are obtained at the surfaces which are both 0.1 mm off the interface for Cu and W .

## Stresses check near the interface at end of the sector

- Model: it is the same as model-2
- The v. M. stresses at end-surface are calculation near the interface at end of sector



## So, we check the paths as following:

$$
\begin{aligned}
& \text { W: } \\
& (-0.2,220,-20.1) \text { to }(-0.2,240,-20.1) \\
& (-0.4,220,-20.1) \text { to }(-0.4,240,-20.1) \\
& (-0.6,220,-20.1) \text { to }(-0.6,240,-20.1) \\
& (-0.8,220,-20.1) \text { to }(-0.8,240,-20.1) \\
& (-1.0,220,-20.1) \text { to }(-1.0,240,-20.1) \\
& \text { Cu } \\
& (-0.2,220,-19.9) \text { to }(-0.2,240,-19.9) \\
& (-0.4,220,-19.9) \text { to }(-0.4,240,-19.9) \\
& (-0.6,220,-19.9) \text { to }(-0.6,240,-19.9) \\
& (-0.8,220,-19.9) \text { to }(-0.8,240,-19.9) \\
& (-1.0,220,-19.9) \text { to }(-1.0,240,-19.9)
\end{aligned}
$$



$$
\begin{aligned}
& \text { W: } \\
& (-1.0,220,-20.2) \text { to }(-1.0,240,-20.2) \\
& (-1.0,220,-20.4) \text { to }(-1.0,240,-20.4) \\
& (-1.0,220,-20.6) \text { to }(-1.0,240,-20.6) \\
& (-1.0,220,-20.8) \text { to }(-1.0,240,-20.8) \\
& (-1.0,220,-21) \text { to }(-1.0,240,-21) \\
& \text { Cu } \\
& (-1.0,220,-19.8) \text { to }(-1.0,240,-19.8) \\
& (-1.0,220,-19.6) \text { to }(-1.0,240,-19.6) \\
& (-1.0,220,-19.4) \text { to }(-1.0,240,-19.4) \\
& (-1.0,220,-19.2) \text { to }(-1.0,240,-19.2) \\
& (-1.0,220,-18) \text { to }(-1.0,240,-18)
\end{aligned}
$$



## v. M. stress for W



$$
\begin{aligned}
& \text { W: } \\
& (-0.2,220,-20.1) \text { to }(-0.2,240,-20.1) \\
& (-0.4,220,-20.1) \text { to }(-0.4,240,-20.1) \\
& (-0.6,220,-20.1) \text { to }(-0.6,240,-20.1) \\
& (-0.8,220,-20.1) \text { to }(-0.8,240,-20.1) \\
& (-1.0,220,-20.1) \text { to }(-01.0,240,-20.1)
\end{aligned}
$$

Along the interface at tungsten


## v. M. stress for Cu



Cu
$(-0.2,220,-19.9)$ to $(-0.2,240,-19.9)$
$(-0.4,220,-19.9)$ to $(-0.4,240,-19.9)$
$(-0.6,220,-19.9)$ to $(-0.6,240,-19.9)$
$(-0.8,220,-20.1)$ to $(-0.8,240,-19.9)$
$(-1.0,220,-19.9)$ to (-1.0, 240, -19.9)
Along the interface at Cu


## v. M. stress for W



W:
$(-1.0,220,-20.2)$ to $(-1.0,240,-20.2)$
$(-1.0,220,-20.4)$ to $(-1.0,240,-20.4)$
$(-1.0,220,-20.6)$ to ( $-1.0,240,-20.6$ )
$(-1.0,220,-20.8)$ to $(-1.0,240,-20.8)$
$(-1.0,220,-21)$ to $(-1.0,240,-21)$

The path at interface is 1 mm far from end section.

Path at interface:


## v. M. stress for Cu



## Comparison and Conclusion

|  |  | Peak tempature $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{array}{\|c\|} \hline \text { Peak v.M } \\ \text { stress (MPa) } \end{array}$ | Stresses at interface (Mpa) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v.M.stress |  | sigma r | sigma phi | sigma z |
|  | interface for $\mathbf{W}$ |  | 377 at W | 251 at W | 40 to 130 | 20 to 120 | -50 to 150 | -15 to 10 |
| Full ring | interface for Cu | 65 to 125 |  |  | -30 to 10 | -140 to -50 | -12 to 0 |
| Sliced ring | interface near center of section for $\mathbf{W}$ | 380 at W | 208 at interface | 40 to 100 | 20 to 80 | 40 to 100 | -3 to 7 |
|  | interface near center of section for Cu |  |  | 80 to 135 | -10 to 25 | -130 to -50 | -2 to 13 |
|  | interface near end surface of section for $\mathbf{W}$ |  |  | 20 to 150 | -90 to 10 | -30 to 15 | -45 to -4 |
|  | interface near end surface of section for $\mathbf{C u}$ |  |  | 90 to 130 | -90 to -30 | -140 to -100 | -5 to 1 |



- Sliced ring suffer much less stress.
- However, we need to pay attention to the interface. This can lead to fatigue and thus to loss of thermal contact.


## Thanks!

